Measurement of ${}^{55}Fe(n,p)$ cross sections by the surrogate-reaction method **for fusion technology applications**

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We have measured the proton decay probabilities of the ${}^{56}Fe^*$ and ${}^{47}Ti^*$ compound systems which are populated by the transfer reactions ${}^{52}Cr({}^{6}Li,d){}^{56}Fe^{*}$ (surrogate of $n + {}^{55}Fe \rightarrow {}^{56}Fe^{*} \rightarrow p + {}^{55}Mn$) and populated by the transfer reactions ⁵²Cr(⁶Li,d)⁵⁶Fe^{*} (surrogate of $n + {}^{55}Fe \rightarrow {}^{56}Fe^* \rightarrow p + {}^{55}Mn$) and ${}^{45}Sc({}^{6}Li, \alpha){}^{47}Ti^*$ (surrogate of $n + {}^{46}Ti \rightarrow {}^{47}Ti^* \rightarrow p + {}^{46}Sc$) reactions, respectively. The ⁵⁵Fe(sections were then obtained in the equivalent neutron energy range of 7.9 to 20.1 MeV within the framework of the surrogate-reaction method. The measured results were compared with predictions of the EMPIRE-3.2.3 statistical model code and various recent evaluated data libraries. The experimental cross-section data on ${}^{55}Fe(n,p)$ are in reasonable agreement with EAF-2010, while the TENDL-2014 and ROSFOND-2010 data show some discrepancies. This study demonstrates the possibility of determining neutron-induced charged particle emission cross sections for unstable radionuclides relevant to fusion technology applications by the surrogate-reaction method.

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The fusion of light nuclei has the potential to become a long-term option for the supply of energy with a moderate impact on the environment. International efforts are presently being made in a coordinated and cooperative manner to build an international thermonuclear experimental reactor (ITER) based on the concept of magnetic confinement of plasma, for net fusion energy production [\[1\]](#page-4-0). Although different isotopes of light elements can be paired to achieve fusion, the deuterium-tritium (D-T) reaction has been identified as the most efficient for fusion devices. For the designing and building of the current fusion reactor a number of materials, both structural and functional, are required to be developed. The environmental and safety aspects of fusion reactors depend significantly on material choices [\[2\]](#page-4-0). Because the materials have to face the high fluence of 14.1 MeV neutrons in the fusion reactor, the structural materials should have low activation, good thermomechanical properties and high radiation resistance. In finalizing the specifications for materials, their development, characterization, production, and suitable fabrication into components is a major challenge. Moreover, these high energy neutrons cause (n, p) and (n, α) reactions with almost all elements, leading to the formation of both helium and hydrogen which can cause serious damage to the structural materials [\[3\]](#page-4-0). Therefore the cross-section data of the neutron-induced reactions with the structural materials have a critical importance on fusion reactor design. Generally

stainless steel (SS) is used as a structural material having Fe, Ni, Cr, Mn, Co, and Nb as its main constituents (in SS316 the content of Fe $\sim 65\%$). The neutron-induced transmutation reactions with these elements in the initial SS composition leads to the formation of large numbers of radionuclides in the mass region ∼50–60 such as ⁵³Mn (T_{1/2} = 3.74 × 10⁶) yr), ⁵⁵Fe ($T_{1/2} = 2.73$ yr), ⁶⁰Fe ($T_{1/2} = 1.5 \times 10^6$ yr), ⁶⁰Co $(T_{1/2} = 5.27 \text{ yr})$, ⁵⁹Ni ($T_{1/2} = 7.6 \times 10^4 \text{ yr}$), and ⁶³Ni ($T_{1/2} =$ 100.1 yr) inside the fusion reactor [\[4\]](#page-4-0). This may lead to significant long-term waste disposal and radiation damage issues [\[5–7\]](#page-4-0). Fusion neutronics studies have been done so far considering only the stable isotopes of Cr, Fe, and Ni. But in a D-T fusion reactor, large amounts of radionuclides will be produced during reactor operation as well as after shutdown, which may affect the neutronics of the reactor $[8]$.

The 55 Fe is a primary dominant radionuclide produced during the operation as well as after shutdown of the fusion reactor by neutron-induced reactions via ${}^{56}Fe(n,2n)$, ${}^{54}Fe(n,\gamma)$, ${}^{59}Co(n,\alpha) {}^{56}Mn(\beta^-) {}^{56}Fe(n,2n)$, and ${}^{58}Ni(n,\alpha)$ as shown by pathways in Fig. [1.](#page-1-0) The exposure of natural iron material in the initial SS composition to high neutron flux will produce high amounts of 55 Fe via the threshold reaction ${}^{56}Fe(n,2n) {}^{55}Fe$ [\[4,7\]](#page-4-0). The activation analysis carried out assuming 1.043×10^{15} n/cm²/s on the first wall during 5 full power years (FPY) on a 1 kg pure iron sample, shows that the ⁵⁵Fe activities are 4.07×10^{14} Bq/kg just after irradiation [\[9\]](#page-4-0). This corresponds to production of ⁵⁵Fe \sim 4.5 gm/kg of pure iron. These nuclei will interact with slow and fast neutrons and produce large amounts of hydrogen and helium which lead to the swelling and embrittlement of the first wall and other structural materials. Therefore the neutroninduced cross sections of the ${}^{55}Fe(n,p)$ ${}^{55}Mn$ reaction are

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FIG. 1. Schematic of ${}^{55}Fe$ formation pathways in typical fusion reactor.

crucial for the fusion reactor from a neutronics point of view [\[10,11\]](#page-4-0).

As of today, there is no direct experimental measurement of the ${}^{55}Fe(n,p)$ cross section because of the unavailability of a ⁵⁵Fe target in nature. When direct experimental determination of compound nuclear cross sections is difficult, indirect methods are often used. The surrogate-nuclear-reaction technique is such an indirect method for determining the compound nuclear cross section for a particular type of "desired" reaction, namely, a two-step reaction, $a + A \rightarrow B^* \rightarrow c + C$, that proceeds through a compound nuclear state B∗. This method was first proposed by Cramer and Britt in the 1970s to estimate neutron-induced fission cross sections from transfer reactions [\[12,13\]](#page-4-0). In a compound reaction, target and projectile nuclei combine to form a highly excited, intermediate system, the compound nucleus, which subsequently decays. The reaction proceeds on a relatively slow time scale $(\gg 10^{-22}$ s), because the formation of a compound nucleus involves the excitation of many degrees of freedom. Apart from observing the constraints of basic conservation laws (energy and angular momentum), the formation and decay of a compound nucleus are considered to be independent of each other in first order which is the Bohr hypothesis. This independence is exploited in the surrogate-reaction approach. Moreover, the surrogate-reaction method also invokes the approximation that the decay of the compound nucleus is independent of the angular momentum and parity of the populated state, which is known as the Weisskopf-Ewing limit of Hauser-Feshbach theory or Weisskopf-Ewing approximation. In such situations, the cross section for the desired reaction can be expressed as $\sigma_{\alpha\beta}(E_{\text{ex}}) = \sigma_{\alpha}^{\text{CN}}(E_{\text{ex}})\Gamma_{\beta}(E_{\text{ex}})$ [\[17,18\]](#page-4-0). Here α denotes the entrance channel $(a + A)$ and β represents the relevant exit channel $(c + C)$. The formation cross section $\sigma_\alpha^{\text{CN}}(E_{\text{ex}}) = \sigma(a + A \rightarrow B^*)$ can be calculated to a reasonable accuracy by using optical potentials, while the theoretical decay probabilities $\Gamma_{\beta}(E_{\text{ex}})$ for the different decay channels β are often quite uncertain. The objective of the surrogate method is to obtain these decay probabilities experimentally. The desired reaction $a + A \rightarrow B^* \rightarrow c + C$ which leads to the compound system B^{*} at an excitation energy (E_{ex}) can decay through different exit channels: fission, gamma-decay, neutron

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and charged particle emission. In a Surrogate experiment, the compound nucleus B^{*} occurring in the desired reaction($a + A$ \rightarrow B^{*} \rightarrow c + C) that involves unstable targets is produced via an alternate (surrogate) direct reaction $(d + D \rightarrow b + B^*)$ which involves a stable projectile-target combination $(d + D)$. The transfer reaction $(d + D \rightarrow b + B^*)$ leads to the formation of compound system B^* and ejectile b. The identification of the ejectile permits one to determine the mass *A* and charge *Z* of the decaying nucleus. In addition, the excitation energy E_{ex} of the nucleus A is determined by employing the two-body kinematics. Also the measurement of the number of coincidences between the ejectiles (b) and the decay channel (β) normalized to the total number of detected ejectiles allows one to extract the decay probability $\Gamma_\beta(E_{\text{ex}}) = \frac{N_{\beta-b}}{N_b}$ for the corresponding decay channel. Within the framework of the surrogate-reaction method, the cross section $\sigma_{\alpha\beta}(E_{\rm ex})$ for the corresponding decay channel β for the desired reaction is then deduced from the product of the decay probability measured in the surrogate reaction and the compound nucleus formation cross section for the desired reaction [\[12\]](#page-4-0), which is obtained from optical model calculations. The compound nucleus excitation energy can be translated into equivalent neutron energy E_n via the relation $E_n = \frac{A+1}{A}(E_{ex} - S_n)$, where S_n is the neutron separation energy of the compound nucleus $[14]$. In a transfer reaction, the residual compound system is populated over a wide range of excitation energy. Therefore, with fixed beam energy, the surrogate method allows one to determine the cross sections over a wide range of equivalent neutron energy.

In recent years, the surrogate-reaction method has been extensively used to determine neutron induced fission cross sections for a large number of actinide targets [\[14–16\]](#page-4-0). Some efforts were also made to determine neutron capture cross sections [\[17,18\]](#page-4-0). But so far no attempts have been made to determine compound nuclear particle emission cross sections using the surrogate-reaction method. In the present work, the ${}^{55}Fe(n,p)$ reaction cross sections have been obtained from measurements of the ratio of proton decay probabilities of ${}^{56}Fe^*$ and ${}^{47}Ti^*$ compound nuclei over the excitation energy range 19–30 MeV. The ${}^{56}Fe^*$ and ${}^{47}Ti^*$ compound nuclei at similar excitation energies are produced in ${}^{52}Cr({}^{6}Li,d){}^{56}Fe*$ and ⁴⁵Sc(⁶Li, α)⁴⁷Ti^{*} transfer reactions at $E_{lab} = 33.0$ and 35.75 MeV, respectively. The cross-section value of the $n + 46$ Ti \rightarrow ⁴⁷ Ti^{*} \rightarrow p +⁴⁶ Sc reaction as a function of excitation energy has been used as the reference to determine the $n +$ ${}^{56}Fe \rightarrow {}^{56}Fe^* \rightarrow p + {}^{55}Mn$ cross section from the measured ratio of the decay probabilities of ${}^{56}Fe^*$ and ${}^{47}Ti^*$ compound systems.

The experiment was performed at Bhabha Atomic Research Centre, Tata Institute of Fundamental Research (BARC-TIFR) 14-MV Pelletron accelerator facility at Mumbai. The selfsupporting thin metallic targets of natCr (abundance $52Cr \sim$ 84%) and ⁴⁵Sc (abundance = 100%) of thickness 500 μ g/cm² prepared by the thermal evaporation technique were bombarded with a ⁶Li beam at incident energies $E_{\text{lab}} = 33.0$ and 35.75 MeV, respectively. The transfer reactions, relevant ground-state Q values (Q_{gg}) , compound nucleus, neutron separation energies, and corresponding surrogate neutroninduced reactions are listed in Table [I.](#page-2-0) The two silicon surface

TABLE I. Transfer reactions investigated in the present experiment, their ground-state Q values (Q_{gg}) and corresponding surrogate neutron-induced reactions.

Transfer	${\cal Q}_{gg}$	CN	S_n	Neutron-induced
reaction	(MeV)		(MeV)	reaction
${}^{52}Cr({}^{6}Li,d)$	6.139	56 Fe	11.197	${}^{55}Fe(n,p)$
45 Sc(6 Li, α)	15.527	47 Ti	13.189	46 Ti (n,p)

barrier (SSB) ΔE -*E* detector telescopes with ΔE detectors of thickness 150 μ m and 100 μ m and identical *E* detectors of thickness of 1 mm were mounted at angles of $25°$ and $35°$ with respect to the beam direction around the transfer grazing angle to identify the projectile-like fragments (PLFs).

The proton, deuteron, triton, and α particles are uniquely identified by plotting ΔE against the residual energy (E_{res}) in the *E* detector. This plot was then converted to a plot of the effective particle identification (PI) versus total energy. This was generated using the linearization function PI= $b(E_{\text{tot}}^{1.70} - E_{\text{res}}^{1.70})$, where E_{tot} is the total particle energy, E_{res} is the energy deposited in the E detector, and b is a constant. Figure 2 shows a typical PI versus total energy plot, where all PLFs are clearly identified. The compound nuclei $56Fe$ and ⁴⁷Ti formed in ⁵²Cr(⁶Li,d)⁵⁶Fe^{*} and ⁴⁵Sc(⁶Li, α)⁴⁷Ti^{*} transfer reactions are identified by outgoing d and α PLFs, respectively. A large area 16-strip solid-state detector (each strip of size 3.1 mm \times 50.0 mm, $\Delta E = 60 \mu$ m, and $E =$ 1500 μ m) was placed at a back angle 130 \degree with respect to the beam direction with an angular opening of 16◦ to detect the decay proton in coincidence with PLFs. The typical outgoing evaporated proton spectra from the compound system ⁵⁶Fe^{*} in coincidence with PLFs (deuteron) is shown in Fig. 3, along with the predictions of statistical model code PACE4 [\[19\]](#page-4-0). It can be seen that PACE4 predictions compare well with the experimental proton spectrum, confirming the evaporation nature of the proton emission. The time correlation between

FIG. 3. Measured proton energy spectra in coincidence with deuteron PLFs at $\theta_{\rm lab} = 130^{\circ}$ for the ⁶Li +⁵² Cr reaction at 33.0 MeV. Also the prediction of PACE4 statistical model is shown as a continuous line.

PLFs and decay particles (protons) are recorded through a time to amplitude converter (TAC). A typical TAC versus PLF deuteron energy plot in ⁶Li+⁵²Cr reaction at $E_{\text{lab}} = 33.0 \text{ MeV}$ is shown in Fig. 4.

The ground-state Q_{gg} for ⁵²Cr(⁶Li,d)⁵⁶Fe^{*} and 45 Sc(6 Li, α) 47 Ti * transfer reactions are 6.139 and 15.527 MeV, respectively. The ${}^{56}Fe^*$ and ${}^{47}Ti^*$ compound systems are populated at overlapping excitation energies in the range of 19–30 MeV in ${}^{6}Li + {}^{52}Cr \rightarrow d + {}^{56}Fe^{*}$ transfer reaction $[E_{\text{lab}}(^{6}\text{Li}) = 33.0 \text{ MeV}]$ and ${}^{6}\text{Li} + {}^{45}\text{Sc} \rightarrow \alpha + {}^{47}\text{Ti}^*$ transfer reaction $[E_{lab}^{\text{(6)}}(L_i) = 35.75 \text{ MeV}]$, respectively. The proton decay probabilities of ⁵⁶Fe^{*} and ⁴⁷Ti^{*} compound nuclei produced in the transfer reactions are obtained from Eq. (1) .

$$
\Gamma_p^{\text{CN}}(E_{\text{ex}}) = \frac{N_{i-p}(E_{\text{ex}})}{N_i(E_{\text{ex}})},\tag{1}
$$

where i denotes the deuteron or α PLF channels corresponding to the ⁵⁶Fe^{$*$} or ⁴⁷Ti^{$*$} compound nucleus. N_i and N_{i−p} denotes the singles and coincidence counts, respectively, at excitation energy E_{ex} .

FIG. 4. Typical PLF-proton TAC versus deuteron (PLF) energy plot in the ⁶Li + ⁵²Cr reaction at $E_{\text{lab}} = 33.0 \text{ MeV}$.

FIG. 5. Excitation energy spectra of the target-like fragments produced in ${}^{6}Li + {}^{52}Cr$ and ${}^{6}Li + {}^{45}Sc$ reactions corresponding to PLF deuteron and alpha with $[(a), (b)]$ and without $[(c), (d)]$ coincidence with evaporated proton.

The telescopes and strip detector were energy calibrated by using the 229 Th source and in an in-beam experiment that made use of ${}^{16}O^*$ excited states formed in the ${}^{12}C({}^{6}Li,$ d ¹⁶O^{*} reaction at 18 MeV. The excitation energy spectra of target-like residues of ${}^{56}Fe^*$ and ${}^{47}Ti^*$ were determined by employing two-body kinematics for deuteron and α PLF channels. The excitation energy spectra so obtained for ${}^{56}Fe$ ^{*} and $47T_1^*$ nuclei are shown in Fig. 5. The excitation energy spectra obtained for PLF-proton coincidence are also shown in the same figure. The ratios of coincidence to single counts were determined in steps of 1.0 MeV excitation energy bin in the energy range 19–30 MeV for ${}^{56}Fe^*$ and ${}^{47}Ti^*$ compound systems. The relative proton decay probabilities for the same excitation energy bin are multiplied with the relative neutron-induced compound nuclear formation cross sections to obtain the ratio of the compound nuclear reaction cross sections as follows:

$$
\frac{\sigma^{^{55}\text{Fe}(n,p)}(E_{\text{ex}})}{\sigma^{^{46}\text{Ti}(n,p)}(E_{\text{ex}})} = R(E_{\text{ex}})
$$
\n
$$
= \frac{\sigma_{\text{CN}}^{n+^{55}Fe}(E_{\text{ex}})}{\sigma_{\text{CN}}^{n+^{46}\text{Ti}}(E_{\text{ex}})} \frac{\Gamma_p^{^{56}\text{Fe}}(E_{\text{ex}})}{\Gamma_p^{^{47}\text{Ti}}(E_{\text{ex}})}.
$$
\n(2)

The ${}^{46}Ti(n, p)$ reaction cross section is used as the reference monitor and taken from IRDFF-1.05 (International Reactor Dosimetry Fusion File) [\[20\]](#page-5-0). The neutron-capture cross sections were calculated by the EMPIRE-3.2.3 code for ${}^{56}Fe^*$ and $47Ti^*$ compound systems in the excitation energy range 19 to 30 MeV. Using Eq. (2) the ${}^{55}Fe(n,p)$ cross section as a function of the excitation energy of ${}^{56}Fe$ ^{*} were obtained over the excitation energy range 19–30 MeV. The excitation energy was converted to equivalent neutron energy in the range of 7.9

FIG. 6. The ⁵⁵Fe(n, p) cross section as a function of equivalent neutron energy along with various evaluation results (in text) and EMPIRE-3.2.3 calculations.

to 20.1 MeV by subtracting the neutron separation energy of ${}^{56}Fe$ (Sn = 11.197 MeV). The present experimental results of ${}^{55}Fe(n,p)$ cross sections as a function of equivalent neutron kinetic energy are shown in Fig. 6.

Statistical model calculations have been carried out using the EMPIRE-3.2.3 code $[21]$ to understand quantitatively the ${}^{55}Fe(n, p)$ reaction cross sections in the neutron energy range 1.0 to 20.0 MeV. The standard Hauser-Feshbach formalism [\[22\]](#page-5-0) was applied to calculate the compound nuclear decay [\[23\]](#page-5-0). The input parameters in the calculations such as nuclear masses, ground-state deformations, discrete energy levels and decay schemes, nuclear level densities, moment of inertia, and γ -ray strength functions are taken from the Reference Input Parameter Library RIPL-3 [\[24\]](#page-5-0). We have used global optical model parameters for both neutrons and protons by Koning and Delaroche [\[25\]](#page-5-0). The level density was calculated using the dynamic approach specific to the EMPIRE code based on the enhanced generalized superfluid model with Mayers-Swiatecki shell corrections, including collective enhancements of the level densities due to nuclear vibrations and rotations. The formalism uses the superfluid Bardeen-Cooper-Schrieffer (BCS) [\[26\]](#page-5-0) model below the critical excitation energy (option of EMPIRE specific level density) and the Fermi gas model for above critical excitation energy. For the present calculations, the level density parameter ATILNO was scaled up by a factor of 1.06 for ${}^{55}Fe$ and scaled down by a factor 0.94 for 55Mn in order to obtain the best fit with the present experimental data at all energies. Proton and neutron emissions compete in the compound nucleus decay: increasing the emission probability of one particle affects the emission of all other particles. Therefore the level densities of both ${}^{55}Fe$ and 55Mn play a role in the estimation of the proton emission cross section. In the absence of detailed measurements of all evaporation channels from the compound system, our choice of the ATILNO parameter deviation of 6% from the default value 1.0 to explain the proton emission cross sections as mentioned above renders minimal changes from the known systematics for all channels. Results from EMPIRE-3.2.3 for excitation function with modified ATILNO values explain the present experimental data which agree with the available data library EAF-2010 [\[27\]](#page-5-0), as shown in Fig. [6.](#page-3-0)

In the Fig. [6,](#page-3-0) there are two curves (thin solid and thick solid) from EMPIRE-3.2.3. The thin solid curve is obtained considering the pure (100%) ${}^{55}Fe(n,p)$ reaction cross section, whereas the thick solid curve corresponds to calculation with inclusion of contributions from other possible channels ⁵³Fe(n, p), ⁵⁶Fe(n, p), and ⁵⁷Fe(n, p) as the ^{nat}Cr $\left[\begin{array}{cc} \n^{50}\text{Cr}(4.345\%) & \n^{52}\text{Cr}(84.0\%) & \n^{53}\text{Cr}(9.50\%) & \n^{54}\text{Cr}(2.365\%) \n\end{array} \right]$ target is used in the present experiment. The theoretically calculated values of EMPIRE-3.2.3 code are in good agreement with our measured values. The present results for the ${}^{55}Fe(n, p)$ cross section by the surrogate-reaction method also follow closely the data files TENDL-2014 [\[28\]](#page-5-0) and ROSFOND-2010 [\[29\]](#page-5-0) between 13 and 20 MeV. In the neutron energy range of 7 to 12 MeV, the measured cross-section data are in reasonable agreement with EAF-2010, while TENDL-2014 and ROSFOND-2010 data show some discrepancy with the present measured data. As expected, this agreement with EAF-2010 is due to the normalization of the evaluation data to 14.5 MeV neutron-induced reactions.

Generally, it is assumed that the production of the hydrogen contribution due to the ${}^{55}Fe(n,p)$ reaction is negligible in fusion reactor calculations. However, its inclusion can lead to an increase in hydrogen generation because the neutroninduced proton emission cross sections at 14 MeV for various isotopes such as ${}^{54}Fe(n,p) \sim 400$ mb [\[30\]](#page-5-0), ${}^{55}Fe(n,p) \sim$ 200 mb (present work), and ⁵⁶Fe(n, p) ~ 140 mb [\[30\]](#page-5-0) are comparable. Therefore, the reactions $54,55,56$ Fe(n, p) compete for hydrogen production.

In summary the ⁵⁵Fe(*n*, *p*) cross sections have been measured in the equivalent neutron energy range of 7.9 to 20.1 MeV

by employing the surrogate-reaction method. The compound nuclei ⁵⁶Fe and ⁴⁷Ti are populated in ⁵²Cr(⁶Li,d)⁵⁶Fe^{*} [surrogate of ⁵⁵Fe(n, p)] and ⁴⁵Sc(⁶Li, α)⁴⁷Ti^{*} [surrogate of $^{46}Ti(n, p)$] transfer reactions. The $^{55}Fe(n, p)$ cross sections are then obtain in the excitation energy range of 19–30 MeV within the framework of the surrogate-reaction method. The known ${}^{46}Ti(n, p)$ cross-section values obtained from the literature have been used as reference. The excitation energy is then converted to equivalent neutron energy by subtracting the neutron separation energy of the $56Fe$ to obtain $55Fe(n,p)$ cross sections in the equivalent neutron energy range of 7.9–20.1 MeV. The experimental results of ${}^{55}Fe(n, p)$ cross sections have been compared with the available evaluation data libraries and EMPIRE-3.2.3 based calculations. By changing the level density parameter by 6% from the default value, the calculated and experimental cross sections are observed to be in good agreement. The present experimental data have also been compared with evaluated data libraries EAF-2010, TENDL-2014, and ROSFOND-2010. The data of the EAF-2010 library are found to be reasonably consistent with the experimental data. The present measurement using the surrogate-reaction method will be useful to improve and update the different data libraries and opens up the possibility of measuring important compound nuclear reactions involving unstable targets with relevance to fusion technology.

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