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R. Mucciola^a, C. Paradela^b, G. Alaerts^b, J. Heyse^b, S. Kopecky^b, C. Massimi^a, P. Schillebeeckx^b and R. Wynants^b

^a Department of Physics and Astronomy, University of Bologna and INFN – Bologna, Italy

^b European Commission, Joint Research Centre, B - 2440 Geel, Belgium

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^a Department of Physics and Astronomy, University of Bologna and INFN – Bologna, Italy

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^aDepartment of Physics and Astronomy, University of Bologna and INFN – Bologna, Italy ^bEuropean Commission, Joint Research Centre, B - 2440 Geel, Belgium

Abstract. Transmission measurements have been performed at the time-of-flight facility GELINA to determine neutron resonance parameters for ^{155,157}Gd. The measurements have been carried out at a 10 m transmission station equipped with a Li-glass scintillator as neutron detector. The accelerator was operated at two frequencies, i.e. 400 Hz and 50 Hz, to cover a broad energy region of the moderated neutron beam. This report provides the experimental details required to deliver the data to the EXFOR data library which is maintained by the International Network of Nuclear Reaction Data Centres (NRDC). In this document, the experimental conditions and data reduction procedures are described. In addition, the full covariance information based on the AGS concept is given such that nuclear reaction model parameters together with their covariances can be derived in a least-squares adjustment to the data.

1 Introduction

To study the resonance structure of neutron-induced reaction cross-sections, neutron spectroscopic measurements are required that determine with a high accuracy the energy of the neutron that interacts with the material under investigation. To cover a broad energy range such measurements are best carried out with a pulsed white neutron source, which is optimized for time-of-flight (TOF) measurements [1].

The TOF-facility GELINA [2][3] has been designed and built for high-resolution crosssection measurements in the resonance region. It is a multi-user facility, providing a white neutron source with a neutron energy range from 10 meV to 20 MeV. Up to 10 experiments can be performed simultaneously at stations located between 10 m to 400 m from the neutron production target. The electron linear accelerator provides a pulsed electron beam with a maximum energy of 150 MeV, a peak current of 10 A and a repetition rate ranging from 50 Hz to 800 Hz. A compression magnet reduces the width of the electron pulses to a Full Width at Half Maximum (FWHM) of about 2 ns [4]. The electron beam hits a mercurycooled uranium target producing Bremsstrahlung and subsequently neutrons via photonuclear reactions [5]. Two water-filled beryllium containers mounted above and below the neutron-producing target are used to moderate the neutrons. By applying different neutron beam collimation conditions, experiments can use either a fast or a moderated neutron spectrum. The neutron production rate is monitored by BF₃ proportional counters, which are mounted in the ceiling of the target hall. The output of these monitors is used to normalize the time-of-flight spectra to the same neutron intensity. The measurement stations are equipped with air conditioning to reduce electronic drifts in the detection chains due to temperature changes. The temperature in the measurement stations is continuously monitored.

In this report, results of transmission measurements carried out at GELINA with ^{155,157}Gd metallic samples are described. To reduce bias effects due to e.g. dead time and background, the measurement and data reduction procedures recommended in Ref. [1] have been followed. The main objective of this report is to provide the information that is required to extract resonance parameters for ^{155,157}Gd in a least squares adjustment to the data using e.g. the resonance shape analysis code REFIT [6]. In the description of the data, the recommendations resulting from a consultant's meeting organized by the Nuclear Data Section of the IAEA have been followed [7].

2 Experimental conditions

The transmission experiments were performed at the 10 m measurement station of flight path 13 with the accelerator operating at 50 Hz and 400 Hz. The moderated neutron spectrum was used. A shadow bar made of Cu and Pb was placed close to the uranium target to reduce the intensity of the γ -ray flash and the fast neutron component. The flight path forms an angle of 18° with the direction normal to the face of the moderator viewing the flight path. The samples and detector were placed in an acclimatized room to keep them at a temperature of about 20°C.

The neutrons scattered from the moderators were collimated into the flight path through an evacuated aluminum pipe of 50 cm diameter with annular collimators, consisting of borated wax, copper and lead. A set of Pb, Ni and Cu annular collimators was used to reduce the neutron beam to a diameter of 10 mm at the sample position. Additional lithium and B₄C collimators were installed to absorb neutrons that are scattered by the collimators [8]. The impact of the γ -ray flash was reduced by a Pb filter placed at the entrance of the station. The samples were placed at 7.7 m distance from the neutron source. The neutron beam passing through the sample and filters was further collimated and detected by a 6.35 mm x 76 mm x 76 mm Scionix Li-glass scintillator. The detector was placed at about 11 m from the neutron target.

Permanent Co and Na black resonance filters were used to continuously monitor the background at 132 eV and 2850 eV, respectively, and to account for the impact of the sample on the background [1]. Additional Ag (5.2 eV) and W (21.1 eV) black resonance filters were included during short cycles to estimate the background shape at lower neutron energies. A 4 mm thick Cd overlap filter was placed in front of the sample position with the accelerator operating at 400 Hz to absorb slow neutrons from a previous burst. The measurements with the accelerator operating at 50 Hz were performed without the overlap filter. The TOF-dependence of the background under these conditions was verified by additional measurements with Rh (1.3 eV), Ag and W black resonance filters in the beam.

The TOF of the detected neutron was derived from the time difference between the stop signal T_s , obtained from the anode pulse of the PMT, and the start signal T_0 , given at each electron burst. This time difference was processed with a multi-hit fast time coder with a 1 ns time resolution. The TOF and the pulse height of each detected event were recorded in list mode using a multi-parameter data acquisition system developed at the EC-JRC [9]. Each measurement was subdivided in different cycles. Only cycles for which the ratio between the total counts in the transmission detector and in the neutron monitor deviated by less than 1 % were selected. The dead time of the detection chain $t_d = 3510$ (10) ns was derived from a spectrum of the time interval between successive events. The maximum dead time correction was less than 20 %. In Ref. [1], it is demonstrated that uncertainties for such dead time corrections are very small and can be neglected.

Measurements were performed with ^{155,157}Gd metallic samples of two different thicknesses. They were sandwiched in two Mylar foils of 6 µm thickness. The thicker samples were measured at an accelerator frequency of 400 Hz to study the low energy resonances, while the thinner samples were measured at 50 Hz to cover the neutron energy region from 10 meV to about 100 eV. The main characteristics of the samples are reported in Table 1 and Table 2. One of the gadolinium samples is shown in Figure 1. The areal density of the samples was derived from a measurement of the weight and the area with an uncertainty better than 0.1 %. The area was determined by an optical surface inspection with a microscope system from Mitutoyo [10]. The sample-out measurements were performed using a dummy Mylar sample made from the same batch that was used to cover the Gd samples.



Figure 1. Picture of one of the gadolinium samples used for the transmission measurements described in this report.

ID	Isotope	Thickness /mm	Mass/mg	Area/mm ²	Areal Density (at/b)
1	¹⁵⁵ Gd	0.0040 (4)	10.0 (1)	313.7 (2)	1.238 (12) x 10 ⁻⁵
2	¹⁵⁵ Gd	0.040 (4)	100.6 (1)	316.4 (1)	12.353 (12) x 10 ⁻⁵
3	¹⁵⁷ Gd	0.0020 (2)	4.7 (1)	315.51 (4)	0.571 (12) x 10 ⁻⁵
4	¹⁵⁷ Gd	0.080 (8)	191.6(1)	315.8 (1)	23.272 (12) x 10 ⁻⁵

Table 1. Characteristics of the samples used for the transmission measurements described in this report. The areal densities were derived from a measurement of the weight and area.

Sample	¹⁵² Gd	¹⁵⁴ Gd	¹⁵⁵ Gd	¹⁵⁶ Gd	¹⁵⁷ Gd	¹⁵⁸ Gd	¹⁶⁰ Gd
¹⁵⁵ Gd	0.03%	0.63%	91.74%	5.12%	1.14%	0.94%	0.4%
¹⁵⁷ Gd	<0.01%	0.04%	0.29%	1.68%	88.32%	9.10%	0.57%

Table 2. Isotopic composition of the enriched gadolinium samples. The data are given in wt%.

3 Data reduction

The AGS code [11][12], developed at JRC-Geel, was used to derive the experimental transmission from the TOF-spectra. The code is based on a compact formalism to propagate both correlated and uncorrelated uncertainties starting from uncorrelated uncertainties due to counting statistics.

3.1 Experimental transmission

The experimental transmission T_{exp} as a function of TOF was obtained from the ratio of a sample-in measurement C_{in} and a sample-out measurement C_{out} , both corrected for their background contributions B_{in} and B_{out} , respectively:

$$T_{exp} = N \frac{C_{in} - KB_{in}}{C_{out} - KB_{out}}.$$
 (3.1)

The TOF spectra (Cin, Cout, Bin, Bout) were corrected for losses due to the dead time in the detector and electronics chain. All spectra were normalized to the same TOF-bin width structure and neutron beam intensity. The latter was derived from the response of the BF₃ beam monitors. To avoid systematic effects due to slow variations of both the beam intensity and detector efficiency as a function of time, data were taken by alternating sample-in and sample-out measurements in cycles. Such a procedure reduces the uncertainty on the normalization to the beam intensity to less than 0.25 %. This uncertainty was evaluated from the ratios of counts in the ⁶Li transmission detector and in the flux monitors. To account for this uncertainty the factor N = 1.0000 (25) was introduced in Eq. (3.1). The background as a function of TOF was approximated by an analytic expression applying the black resonance technique [1]. The factor K = 1.00 (3) in Eq. (3.1) was introduced to account for systematic effects due to the background model. Its uncertainty was derived from a statistical analysis of the difference between the observed black resonance dips and the estimated background [13]. This uncertainty is only valid for measurements with at least two fixed black resonance filters placed in the beam [1].

The time-of-flight (t) of a neutron creating a signal in the neutron detector was determined by the time difference between the stop signal (T_s) and the start signal (T_0):

$$t = (T_s - T_0) + t_0, (3.2)$$

with t_0 a time-offset which was determined by a measurement of the γ -ray flash. The flight path distance L = 10.861 (1) m, i.e. the distance between the center of the moderator viewing the flight path and the front face of the detector, was derived from results of transmission measurements using a uranium sample and the resonance energies for ²³⁸U+n reported by Derien et al. [14].

3.2 Background correction

The background contribution for the transmission measurements was approximated by an analytical function applying the black resonance technique [1]. The analytical function was a sum of a time-independent and three time-dependent components:

B (t) =
$$b_0 + b_1 e^{-\lambda_1 t} + b_2 e^{-\lambda_2 t} + b_3 e^{-\lambda_3 (t+\tau_0)}$$
. (3.3)

The time-independent component b_0 is related to the ambient radiation and background contributions that lost any time correlation. The first exponential term is due to the detection of 2.2 MeV γ -rays resulting from neutron capture in hydrogen present in the moderator. The second exponential term originates predominantly from neutrons scattered inside the detector station. The third one is attributable to slow neutrons from previous accelerator cycles. This contribution was estimated by an extrapolation of the

TOF-spectrum at the end of the cycle. The time shift τ_0 is the inverse of the accelerator frequency, i.e. $\tau_0 = 2.5$ ms for 400 Hz and $\tau_0 = 20$ ms for 50 Hz. The decay constants λ_1 and λ_2 were derived from results of measurements with additional background filters in the beam combined with the data of measurements with a 3 mm thick Au sample. The dead time corrected sample-in TOF-spectrum together with the background contributions resulting from the measurements with the thin ¹⁵⁷Gd sample and Na, Co, W, Ag and Rh black resonance filters is shown in Figure 2. These data were obtained with the accelerator operating at 50 Hz. The TOF-spectrum resulting from measurements with the thick ¹⁵⁵Gd sample and Na, Co, W and Ag filters with the accelerator operated at 400 Hz is shown in Figure 3. The parameters of the background components for the measurements discussed in this report are given in Table 3 – Table 6.

ID	b ₀ /10 ⁻⁹ ns ⁻¹	b1/10 ⁻⁶ ns ⁻¹	$\lambda_{1}/10^{-5}$ ns ⁻¹	b2/10 ⁻⁸ ns ⁻¹	λ ₂ /10 ⁻⁶ ns ⁻¹	b₃/10⁻ ⁶ ns⁻¹	λ ₃ /10 ⁻⁷ ns ⁻¹
Bin	1.29	1.00	3.00	7.14	2.18	1.91	5.27
Bout	1.29	1.06	3.00	7.89	2.18	2.36	4.26

Table 3. Parameters for the analytical expressions of the background components for sample-in (0.004 mm thick ¹⁵⁵Gd sample) and sample-out measurements. The parameters are derived from results of measurements with Na and Co black resonance filters in the beam and the accelerator operating at 50 Hz.

ID	b₀/10 ⁻⁹ ns ⁻¹	b1/10 ⁻⁷ ns ⁻¹	λ ₁ /10 ⁻⁵ ns ⁻¹	b2/10 ⁻⁸ ns ⁻¹	λ ₂ /10 ⁻⁶ ns ⁻¹	b3/10 ⁻⁶ ns ⁻¹	λ ₃ /10 ⁻⁷ ns ⁻¹
Bin	1.26	9.47	3.00	7.35	2.29	1.53	5.96
Bout	1.26	9.24	3.00	7.56	2.29	2.26	4.30

Table 4. Parameters for the analytical expressions of the background components for sample-in (0.002 mm thick ¹⁵⁷Gd sample) and sample-out measurements. The parameters are derived from results of measurements with Na and Co black resonance filters in the beam and the accelerator operating at 50 Hz.

ID	b₀/10 ⁻⁹ ns ⁻¹	b1/10 ⁻⁶ ns ⁻¹	$\lambda_{1}/10^{-5}$ ns ⁻¹	b2/10 ⁻⁷ ns ⁻¹	λ ₂ /10 ⁻⁶ ns ⁻¹	b₃/10 ⁻⁸ ns⁻¹	λ ₃ /10 ⁻⁷ ns ⁻¹
Bin	1.29	1.09	2.40	3.51	4.50	9.44	5.31
Bout	1.29	1.08	2.40	3.63	4.50	9.47	5.31

Table	e 5. Parai	meter	s for th	e ana	alytical	express	sions	of the	backg	round	l compo	nents	for sa	mple-in	(0.04	mm	thick
¹⁵⁵ Go	sample)) and s	sample	-out	measur	ements	s. Th	ie para	meters	s are	derived	from	results	s of mea	asuren	nents	with
a Cd	overlap	filter a	nd Na	and	Co blac	k reson	ance	filters	in the	beam	n and th	e acce	elerato	r opera	ting at	400	Hz.

ID	b ₀ /10 ⁻⁹ ns ⁻¹	b ₁ /10 ⁻⁶ ns ⁻¹	$\lambda_{1}/10^{-5}$ ns ⁻¹	b ₂ /10 ⁻⁷ ns ⁻¹	λ ₂ /10 ⁻⁶ ns ⁻¹	b ₃ /10 ⁻⁸ ns ⁻¹	λ ₃ /10 ⁻⁷ ns ⁻¹
Bin	1.29	1.07	2.40	3.51	4.50	9.23	5.28
Bout	1.29	1.07	2.40	3.56	4.50	9.27	5.29

Table 6. Parameters for the analytical expressions of the background components for sample-in (0.08 mm thick ¹⁵⁷Gd sample) and sample-out measurements. The parameters are derived from results of measurements with a Cd overlap filter and Na and Co black resonance filters in the beam and the accelerator operating at 400 Hz.



Figure 2. TOF-spectrum resulting from measurements with the ^{157}Gd sample and Na, Co, W, Ag and Rh black resonance filters in the beam and the accelerator operated at 50 Hz. The sample-in spectrum (C_{in}) is shown together with the total background (B_{in}) and its components.



Figure 3. TOF-spectrum resulting from measurements with the 155 Gd sample, Na, Co, W and Ag black resonance filters and Cd overlap filter in the beam and the accelerator operated at 400 Hz. The sample-in spectrum (C_{in}) is shown together with the total background (B_{in}) and its components.

4 Results

The AGS code [11][12] was used to derive the experimental transmission and propagate both the correlated and uncorrelated uncertainties. The code is based on a compact formalism to propagate all uncertainties starting from uncorrelated uncertainties due to counting statistics. It stores the full covariance information after each operation in a concise, vectorized way. The AGS formalism results in a substantial reduction of data storage volume and provides a convenient structure to verify the various sources of uncertainties through each step of the data reduction process. The concept is recommended by the NDS/IAEA [7] to prepare the experimental observables, including their full covariance information, for storage into the EXFOR data library [15][16].

The format in which the numerical data is stored in the EXFOR data library is illustrated in the Appendix. The data include the full covariance information based on the AGS concept. The total uncertainty and the uncertainty due to uncorrelated components are reported, together with the contributions due to the normalization and background subtraction. Applying the AGS concept the covariance matrix V of the experimental transmission can be calculated by:

$$V = U_{u} + S(\eta)S(\eta)^{T}, \qquad (4.2)$$

where U_u is a diagonal matrix containing the contribution of all uncorrelated uncertainty components. The matrix S contains the contribution of the components $\eta = \{N, K\}$ creating correlated components. The uncertainty due to the dead time correction can be neglected. The experimental details, which are required to perform a resonance analysis on the data, are summarized in the Appendix.

Examples of experimental transmissions as a function of neutron energy are shown in Figure 4 and Figure 5. The experimental data obtained in this work are compared with results of calculations using the resonance shape analysis code REFIT with the resonance parameters recommended in ENDF/B-VIII.0 [17], JEFF-3.3 [18] and JENDL-4.0 [19]. For these calculations the TOF-response functions of GELINA reported in Ref. [20] were used. The experimental transmission obtained with the 0.002 mm thick ¹⁵⁷Gd sample and the accelerator operated at 50 Hz is shown in Figure 4 together with the calculated ones. Figure 5 compares the experimental and calculated transmission through the 0.04 mm thick ¹⁵⁵Gd sample for an accelerator frequency of 400 Hz. The residuals in these figures reveal that a new evaluation is required to describe the experimental data reported in this work.



Figure 4. Transmission as a function of neutron energy resulting from measurements with the 0.002 mm thick 157 Gd sample and the accelerator operated at 50 Hz. The experimental transmission (T_{exp}) is compared with the calculated transmission (T_M) using the parameters recommended in the ENDF/B-VIII.0, JEFF-3.3 and JENDL-4.0 libraries. The REFIT code was used to obtain the calculated transmissions.



Figure 5. Transmission as a function of neutron energy resulting from measurements with the 0.04 mm thick 155 Gd sample and the accelerator operated at 400 Hz. The experimental transmission (T_{exp}) is compared with the calculated transmission (T_M) using the parameters recommended in the ENDF/B-VIII.0, JEFF-3.3 and JENDL-4.0 libraries. The REFIT code was used to obtain the calculated transmissions.

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Appendix

A. SUMMARY OF EXPERIMENTAL DETAILS

A. 1 Experiment description (ID 1)

1.	Main Reference		[a]
2.	Facility	GELINA	[b][c]
3.	Neutron production		
	Neutron production beam	Electron	
	Nominal average beam energy	100 MeV	
	Nominal average current	3 μΑ	
	Repetition rate (pulses per second)	50 Hz	
	Pulse width	2 ns	
	Primary neutron production target	Mercury cooled depleted uranium	
	Target nominal neutron production intensity	3.4 x10 ¹³ s ⁻¹	
4.	Moderator		
	Primary neutron source position in	Above and below uranium target	
	moderator		
	Moderator material	2 Water filled Be-containers around U-	
	Moderator dimensions (internal)	2 x (14.6 cm x 21 cm x 3.9 cm)	
	Density (moderator material)	1 g/cm ²	
	Temperature (K)	Room temperature	
	Moderator-room decoupler (Cd, B,)	None	
5.	Other experimental details		
	Measurement type	Transmission	
	Method (total energy, total absorption,)	Good transmission geometry	[d]
	Flight Path length (m)	L = 10.861 (1) m	
	(moderator center-detector front face)		
	Flight path direction	moderator face viewing the flight path	
	Neutron beam dimensions at sample	10 mm in diameter	
	position		
	Neutron beam profile	-	
	Overlap suppression	None	
	Other fixed beam filters	Na, Co, Pb	
6.	Detector		
	Туре	Scintillator	
	Surface Dimensions	76 mm x 76 mm square	
	Detector(c) position relative to neutron		
	beam	In the beam	
	Detector(s) solid angle	-	
7.	Sample		
	Type (metal, powder, liquid, crystal)	Metal	
	Chemical composition	Gd (100 %)	
	Isotopic composition (wt%)	¹⁵² Gd (0.03 %), ¹⁵⁴ Gd (0.63 %), ¹⁵⁵ Gd	
		$(91.74\%),^{156}$ Gd $(5.12\%),^{157}$ Gd	
	Sample composition (at/b)	(1.14%), ¹²⁵ Gd (0.94%) ¹²⁶ Gd (0.4%) 1.238 (12) x 10 ⁻⁵ at/b of ¹⁵⁵ Gd	
	Temperature	20°C	
		=	l

	Sample mass (g)	10.0 (1) mg	
	Geometrical shape (cylinder, sphere,)	Disk	
	Surface dimension	313.7 (2) mm ²	
	Nominal thickness (mm)	0.004 mm	
	Containment description	Sandwiched in 6 μ m Mylar foils	
8.	Data Reduction Procedure		[d][e]
	Dead time correction	Done (< factor 1.2)	
	Background subtraction	Black resonance technique	
	Flux determination (reference reaction,)	-	
	Normalization	1.0000 (25)	
	Detector efficiency	-	
	Self-shielding	-	
	Time-of-flight binning	Zone length bin width 4096 2 ns 5120 4 ns 5120 8 ns 4096 16 ns 4096 32 ns 4096 64 ns 12288 128 ns 4096 512 ns 1024 2048 ns 1024 4096 ns 20480 8192 ns	
9.	Response function	Normal distribution EW/HM - 2 as	
	Target / moderator assembly	Numerical distribution from MC	[f][a]
	rarger / moderator assembly	simulations	[1][3]
	Detector	Analytical function defined in REFIT manual	[h]

A. 2 Experiment description (ID 2)

1.	Main Reference		[a]
2.	Facility	GELINA	[b][c]
3.	Neutron production		
	Neutron production beam	Electron	
	Nominal average beam energy	100 MeV	
	Nominal average current	30 μ A	
	Repetition rate (pulses per second)	400 Hz	
	Pulse width	2 ns	
	Primary neutron production target	Mercury cooled depleted uranium	
	Target nominal neutron production intensity	3.4 x10 ¹³ s ⁻¹	
4.	Moderator		
	Primary neutron source position in moderator	Above and below uranium target	
	Moderator material	2 water filled Be-containers around U- target	
	Moderator dimensions (internal)	2 x (14.6 cm x 21 cm x 3.9 cm)	
	Density (moderator material)	1 g/cm ²	
	Temperature (K)	Room temperature	
	Moderator-room decoupler (Cd, B,)	None	
5.	Other experimental details		
	Measurement type	Transmission	
	Method (total energy, total absorption,)	Good transmission geometry	[d]
	Flight Path length (m)	L = 10.861 (1) m	
	Flight path direction	18° with respect to normal of the	
		moderator face viewing the flight path	
	Neutron beam dimensions at sample	10 mm in diameter	
	position Neutron beam profile	-	
	Overlan suppression	4 mm Cd overlan filter	
	Other fixed beam filters	Na. Co. Ph	
6.	Detector		
		Scintillator	
	Material	Li-glass	
	Surface Dimensions	76 mm x 76 mm square	
	Thickness (cm)	6.35 mm	
	Detector(s) position relative to neutron	In the beam	
	beam		
	Detector(s) solid angle	-	
7.	Sample		
	Type (metal, powder, liquid, crystal)	Metal	
	Chemical composition	Gd (100 %)	
	Isotopic composition (wt%)	152 Gd (0.03 %), 154 Gd (0.63 %), 155 Gd (91.74 %), 156 Gd (5.12 %), 157 Gd (1.14 %), 158 Cd (0.04 %), 160 Cd (0.4 %)	
	Sample composition (at/b)	$12.353 (12) \times 10^{-5} \text{ at/b of } ^{155}\text{Gd}$	
	Temperature	20°C	
	Sample mass (g)	100.6 (1) mg	
	Geometrical shape (cylinder, sphere,)	Disk	
	Surface dimension	316.4 (1) mm ²	
		1	1

	Nominal thickness (mm)	0.04 mm	
	Containment description	Sandwiched in 6 $\mu{ m m}$ Mylar foils	
8.	Data Reduction Procedure		[d][e]
	Dead time correction	Done (< factor 1.2)	
	Background subtraction	Black resonance technique	
	Flux determination (reference reaction,)	-	
	Normalization	1.0000 (25)	
	Detector efficiency	-	
	Self-shielding	-	
	Time-of-flight binning	Zone length bin width 4096 2 ns 5120 4 ns 5120 8 ns 4096 16 ns 4096 32 ns 4096 64 ns 5120 128 ns 4096 512 ns 1024 2048 ns 1024 4096 ns 27648 8192 ns	
9.	Response function		
	Initial pulse	Normal distribution, $FWHM = 2 ns$	
	Target / moderator assembly	Numerical distribution from MC	[f][g]
	Detector	Analytical function defined in REFIT manual	[h]

A. 3 Experiment description (ID 3)

1.	Main Reference		[a]
2.	Facility	GELINA	[b][c]
3.	Neutron production		
	Neutron production beam	Electron	
	Nominal average beam energy	100 MeV	
	Nominal average current	3 μΑ	
	Repetition rate (pulses per second)	50 Hz	
	Pulse width	2 ns	
	Primary neutron production target	Mercury cooled depleted uranium	
	Target nominal neutron production intensity	3.4 x10 ¹³ s ⁻¹	
4.	Moderator		
	Primary neutron source position in moderator	Above and below uranium target	
	Moderator material	2 water filled Be-containers around U-	
	Moderator dimensions (internal)	target $2 \times (14.6 \text{ cm} \times 21 \text{ cm} \times 3.9 \text{ cm})$	
	Density (moderator material)	1 a/cm^2	
	Temperature (K)	Room temperature	
	Moderator-room decoupler (Cd_B)	None	
5	Other experimental details		
5.	Measurement type	Transmission	
	Method (total energy total absorption)	Good transmission geometry	[4]
	Flight Path length (m)	L = 10.861 (1) m	[~]
	(moderator center-detector front face)		
	Flight path direction	18° with respect to normal of the	
	Neutron beam dimensions at sample	moderator face viewing the flight path	
	position		
	Neutron beam profile	-	
	Overlap suppression	None	
	Other fixed beam filters	Na, Co, Pb	
6.	Detector		
	Туре	Scintillator	
	Material	Li-glass	
	Surface Dimensions	76 mm x 76 mm square	
	Thickness (cm)	6.35 mm	
	Detector(s) position relative to neutron	In the beam	
	Detector(s) solid angle	-	
7.	Sample		
	Type (metal, powder, liquid, crystal)	Metal	
	Chemical composition	Gd (100 %)	
	Isotopic composition (wt%)	¹⁵² Gd (<0.01 %), ¹⁵⁴ Gd (0.04 %), ¹⁵⁵ Gd	
		(0.29 %), ¹⁵⁶ Gd (1.68 %), ¹⁵⁷ Gd (88.32 %), ¹⁵⁸ Gd (9.10 %) ¹⁶⁰ Gd (0.57 %)	
	Sample composition (at/b)	0.571 (12) x 10 ⁻⁵ at/b of ¹⁵⁷ Gd	
	Temperature	20°C	
	Sample mass (g)	4.7 (1) mg	
	Geometrical shape (cylinder, sphere,)	Disk	
	Surface dimension	315.51 (4) mm ²	
		1	1

	Nominal thickness (mm)	0.002 mm	
	Containment description	Sandwiched in 6 μ m Mylar foils	
8.	Data Reduction Procedure		[d][e]
	Dead time correction	Done (< factor 1.2)	
	Background subtraction	Black resonance technique	
	Flux determination (reference reaction,)	-	
	Normalization	1.0000 (25)	
	Detector efficiency	-	
	Self-shielding	-	
	Time-of-flight binning	Zone length bin width 4096 2 ns 5120 4 ns 5120 8 ns 4096 16 ns 4096 32 ns 4096 64 ns 12288 128 ns 4096 512 ns 1024 2048 ns 1024 4096 ns 20480 8192 ns	
9.	Response function		
	Initial pulse	Normal distribution, FWHM = 2 ns	
	Target / moderator assembly	Numerical distribution from MC	[f][g]
	Detector	Analytical function defined in REFIT manual	[h]

A. 4 Experiment description (ID 4)

1	Main Reference		[a]
2	Facility	GFLINA	[b][c][
			3]
3.	Neutron production		
	Neutron production beam	Electron	
	Nominal average beam energy	100 MeV	
	Nominal average current	30 µ A	
	Repetition rate (pulses per second)	400 Hz	
	Pulse width	2 ns	
	Primary neutron production target	Mercury cooled depleted uranium	
	Target nominal neutron production intensity	3.4 x10 ¹³ s ⁻¹	
4.	Moderator		
	Primary neutron source position in	Above and below uranium target	
	moderator		
	Moderator material	2 water filled Be-containers around U-	
	Moderator dimensions (internal)	2 x (14.6 cm x 21 cm x 3.9 cm)	
	Density (moderator material)	1 g/cm^2	
	Temperature (K)	Room temperature	
	Moderator-room decoupler (Cd. B.)	None	
5.	Other experimental details		
•	Measurement type	Transmission	
	Method (total energy total absorption)	Good transmission geometry	[4]
	Flight Path length (m)	L = 10.861 (1) m	[0]
	(moderator center-detector front face)		
	Flight path direction	18° with respect to normal of the	
	Noutron beam dimensions at cample	moderator face viewing the flight path	
	position		
	Neutron beam profile	-	
	Overlap suppression	4 mm Cd overlap filter	
	Other fixed beam filters	Na, Co, Pb	
6.	Detector		
	Туре	Scintillator	
	Material	Li-glass	
	Surface Dimensions	76 mm x 76 mm square	
	Thickness (cm)	6.35 mm	
	Detector(s) position relative to neutron	In the beam	
	beam		
	Detector(s) solid angle	-	
7.	Sample		
	Type (metal, powder, liquid, crystal)	Metal	
	Chemical composition	Gd (100 %)	
	Isotopic composition (wt%)	152 Gd (<0.01 %), 154 Gd (0.04 %), 155 Gd	
		(0.29 %), ¹³⁸ Gd (1.08 %), ¹³⁷ Gd (88 32 %) ¹⁵⁸ Gd (9 10 %) ¹⁶⁰ Gd	
		(0.57 %)	
	Sample composition (at/b)	23.272 (12) x 10 ⁻⁵ at/b of ¹⁵⁷ Gd	
	Temperature	20°C	
	Sample mass (g)	191.6 (1) mg	
	Geometrical shape (cylinder, sphere,)	Disk	
	Surface dimension	315.8 (1) mm ²	

	Nominal thickness (mm)	0.08 mm	
	Containment description	Sandwiched in 6 $\mu{ m m}$ Mylar foils	
8.	Data Reduction Procedure		[d][e]
	Dead time correction	Done (< factor 1.2)	
	Background subtraction	Black resonance technique	
	Flux determination (reference reaction,)	-	
	Normalization	1.0000 (25)	
	Detector efficiency	-	
	Self-shielding	-	
	Time-of-flight binning	Zone length bin width 4096 2 ns 5120 4 ns 5120 8 ns 4096 16 ns 4096 32 ns 4096 64 ns 5120 128 ns 4096 512 ns 1024 2048 ns 1024 4096 ns 27648 8192 ns	
9.	Response function		
	Initial pulse	Normal distribution, $FWHM = 2 ns$	
	Target / moderator assembly	Numerical distribution from MC	[f][g]
	Detector	Analytical function defined in REFIT manual	[h]

B. Data format

Column	Content	Unit	Comment
1	Energy	eV	Relativistic relation using a fixed flight path length
			(L = 10.861 m)
2	tı	ns	Low bound
3	t _h	ns	High bound
4	T _{exp}		Transmission
5	Total Uncertainty		
6	Uncorrelated		Uncorrelated uncertainty due to counting statistics
	uncertainty		
7	AGS-vector (K)		Background model uncertainty ($u_K/K=3$ %)
8	AGS-vector (N)		Normalization $(u_N/N = 0.25 \%)$

Comments from the authors:

- The AGS concept was used to derive the experimental transmission

$$T_{exp} = N \frac{C_{in} - KB_{in}}{C_{out} - KB_{out}},$$

and to propagate the uncertainties, both the uncorrelated due to counting statistics and the uncertainty due to the normalization and the background contributions.

- The quoted uncertainties are standard uncertainties at 1 standard deviation.

B.1 DATA (ID 1)

E/ oV/	t/ nc	t, / nc	т	21	AGS		
L/ EV	u / 115	th / IIS	Texp	u _t	u _u	K	N
100.030400	78496	78512	1.031059	0.125505	0.125478	0.000098	0.002578
99.989610	78512	78528	1.068249	0.129550	0.129522	0.000133	0.002671
0.025045	4960256	4962304	0.484828	0.018750	0.018711	0.000030	0.001212
0.025025	4962304	4964352	0.454227	0.017809	0.017773	0.000032	0.001136
0.025004	4964352	4966400	0.495578	0.019395	0.019355	0.000031	0.001239
0.024983	4966400	4968448	0.499244	0.019362	0.019322	0.000030	0.001248
0.005011	11087872	11096064	0.297100	0.042872	0.042842	0.001429	0.000743
0.005003	11096064	11104256	0.306371	0.040337	0.040311	0.001232	0.000766

B.2 DATA (ID 2)

E/ eV	t/ / ns	t _h / ns	T _{exp}	u_t	u_u	AGS K	Ν
350.075600	41960	41968	1.041797	0.021763	0.021606	0.000149	0.002604
349.942200	41968	41976	0.984469	0.020488	0.020340	-0.000016	0.002461
20.97447	171424	171456	0.659020	0.009840	0.009687	-0.000529	0.001648
20.96665	171456	171488	0.658862	0.009840	0.009686	-0.000530	0.001647

6.305760	312640	312704	0.669775	0.008064	0.007876	-0.000428	0.001674
6.303179	312704	312768	0.670058	0.008091	0.007904	-0.000430	0.001675
2.571436	489600	489664	0.383917	0.006327	0.006211	-0.000727	0.000960
2.570764	489664	489728	0.386970	0.006357	0.006241	-0.000723	0.000967
1.000507	784896	785024	0.997266	0.011721	0.011453	0.000007	0.002493
 1.000181	785024	785152	0.998477	0.011724	0.011455	0.00008	0.002496

B.3 DATA (ID 3)

F/		/oV/t/nc/t/nc/T/u/	24	AGS				
	L/ EV	ų / IIS	t _h / 115	l exp	u_t	u_u	K	Ν
	100.030400	78496	78512	0.939886	0.065534	0.065492	-0.000049	0.002350
	99.989610	78512	78528	0.969793	0.068495	0.068452	-0.000026	0.002424
	0.025025	4962304	4964352	0.291784	0.007753	0.007719	-0.000045	0.000729
	0.025004	4964352	4966400	0.277983	0.007472	0.007439	-0.000046	0.000695
	0.024983	4966400	4968448	0.270747	0.007379	0.007348	-0.000047	0.000677
	0.024963	4968448	4970496	0.288086	0.007683	0.007649	-0.000046	0.000720
	0.005011	11087872	11096064	0.107683	0.014458	0.014350	-0.001742	0.000269
	0.005003	11096064	11104256	0.118903	0.014786	0.014687	-0.001682	0.000297

B.4 DATA (ID 4)

	t. / 22	t. / no	Ŧ			AGS	
E/ ev	u / ns	t_h / ns	l exp	u_t	u_u	К	Ν
350.075600	41960	41968	0.926577	0.017810	0.017658	-0.000194	0.002316
349.942200	41968	41976	0.932932	0.017911	0.017757	-0.000176	0.002332
44.08875	118240	118256	0.813762	0.013525	0.013367	-0.000330	0.002034
44.07682	118256	118272	0.814717	0.013569	0.013411	-0.000330	0.002037
16.78164	191648	191680	0.265490	0.005249	0.005086	-0.001118	0.000664
16.77603	191680	191712	0.278353	0.005371	0.005212	-0.001096	0.000696
2.828553	466816	466880	0.695397	0.008364	0.008174	-0.000355	0.001738
2.827778	466880	466944	0.695247	0.008377	0.008187	-0.000356	0.001738
1.000507	784896	785024	0.943179	0.010095	0.009815	-0.000072	0.002358
1.000181	785024	785152	0.954873	0.010255	0.009974	-0.000056	0.002387

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Nuclear Data Section International Atomic Energy Agency P.O. Box 100 A-1400 Vienna Austria e-mail: nds.contact-point@iaea.org fax: (43-1) 26007 telephone: (43-1) 2600 21725 Web: http://nds.iaea.org/